# VALVE PERFORMANCE TEST ON A 4-INCH RUBBER CHECK VALVE 

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## UTAH WATER RESEARCH LABORATORY

# VALVE PERFORMANCE TEST ON A 4-INCH RUBBER CHECK VALVE 

Submitted to:

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## INTRODUCTION

Utah State University was contracted by WAPRO to perform a flow test at the Utah Water Research Laboratory (UWRL) in Logan, Utah on a 4-inch rubber check valve manufactured by WAPRO. A cold-water test was performed to determine the discharge coefficient $(\mathrm{Cv})$ for the valve over a wide range of flow rates under both free discharge and submerged conditions. Tests were also performed to determine the head necessary to open and close the valve.

## EXPERIMENT SETUP

The valve was installed in a 6-inch supply line, which included more than 40 pipe diameters of standard schedule 4 -inch carbon steel laboratory pipe (4.026-inch ID) installed immediately upstream of the valve. A pressure tap was installed on the invert of the pipe at approximately 2 diameters upstream of the valve. Laboratory instrumentation was connected to the pressure tap so that differential pressure measurements during the test could be documented. Discharge from the valve was released to a wooden box, in which water levels could be controlled. Figure 1 and Figure 2 illustrate the freedischarge and submerged tests respectively.


Figure 1. Test Setup for the Free-Discharge 4-Inch Rubber Check Valve Tests


Figure 2. Test Setup for the Submerged 4-Inch Rubber Check Valve Tests

## FLOW COEFFICIENT

The coefficient Cv for the valve was calculated using the following equation:

$$
C v=\frac{Q}{\sqrt{\Delta P / s g}}
$$

in which Q is the actual flow rate in gallons per minute, $\Delta \mathrm{P}$ is the gross valve differential pressure reading in pounds per square inch (psi) and sg is the specific gravity of water during this test ( $\mathrm{sg}=1.0010$ ).

## PROCEDURE

Water was supplied to the test line from a reservoir near the hydraulics laboratory. The flow rate and differential pressure were measured for each run. The water temperature was also measured. During the free discharge tests, the differential pressure measurement across the valve was determined by measuring the difference between the upstream pressure at the pipe pressure tap located at two diameters upstream of the valve and the downstream pressure for the free-discharging valve ( 0 psi at atmospheric pressure). During the submerged discharge tests, the differential pressure measurement across the valve was determined by measuring the difference between the upstream pressure at the pipe pressure tap located at two diameters upstream of the valve and the measured tail water level in the receiving water downstream of the valve. The pressure tap for the tail water level was located in a corner of the box where no velocities existed.

All flow measurements were made using either a calibrated 1 -inch or 6 -inch master laboratory magnetic flow meter installed upstream of the test valve. The calibration for each magnetic flow meter was previously performed using the laboratory weight tanks. The weight tank is regularly calibrated and is traceable to the National Institute of Standards and Technology. Discharge from the test line was controlled using a control valve upstream of the test section.

Valve differentials were measured using a Rosemount differential transmitter. The Rosemount transmitter was carefully zeroed to the invert of the pipe. The transmitter output was averaged during each individual run using an averaging Fluke volt/amp meter. Appropriate ranges were set on the transmitter to minimize uncertainties as the valve differentials changed.

The valve was tested over a wide range of flow rates. The differential pressure and the flow rate were accurately measured and the Cv was calculated for each run. The average Cv is provided in the data table. The head at which the valve just opens and just closes was also determined. Three data points were measured and averaged under both conditions. All instrumentation used is regularly calibrated and traceable to the National Institute of Standards and Technology.

## RESULTS

The head necessary to open the valve was found to be 0.30 ft . The head necessary to close the valve was found to be 0.19 ft . Table 1 and Table 2 summarize the test results for the valve test. Table 1 includes the free-discharge test data and Table 2 includes the submerged test data. Within each table, hysteresis data is also presented. It was determined that slowly increasing the flow produced different results (upper curve) than when the flow was slowly decreasing (lower curve). Figure 3 illustrates the relationship between flow rate and the Cv for the valve with increasing flow. Figure 4 illustrates additional points when the flow rate was slowly decreased. Video clips of specific runs are provided separately.

Table 1. Utah Water Research Laboratory Flow Meter Calibration Data


Certified by:


Research Associate Professor

Table 2. Utah Water Research Laboratory Flow Meter Calibration Data

| Manufacturer: |  | WAPRO |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Calibration Date: |  | 2/22/16 |  |  |  |  |  |
| Calibration Location: |  | 6 -inch supply line |  | Valve Inside Diameter (in.) = Nominal Pipe Dia. = |  | 4.026 |  |
|  |  | 4-inch |  |  |  |
| Serial Number: |  |  |  | NA |  | Pipe Diameter (in.) = |  | 4.026 |  |
| Valve Description: |  | NA |  | Water Temp. (F) = |  | 0.09 |  |
|  |  | 39.2 |  |  |  |
| Pipe Setup |  |  |  | 4-inch std. wall steel pipe |  | Unit Weight (lb/ft ${ }^{3}$ ) $=$ <br> Kin. Visc. $\left(\mathrm{ft}^{2} / \mathrm{s}\right)=$ |  | 62.43 |  |
| Upstream: Downstream: |  | $1.69 \mathrm{E}-05$ |  |  |  |  |  |
|  |  | 4 -inch std. wall steel pipe |  |  |  |  |  |
| Calibration Performed by: Calibration Witnessed by: |  | Z. Sharp none |  |  |  |  |  |
|  |  |  | Inlet | $\begin{aligned} & \text { Flow } \\ & \text { Area } \\ & \mathrm{ft}^{\wedge} 2 \\ & \hline \end{aligned}$ |  | Pipe | Cv |
| Run No. | Flow gpm | $\begin{gathered} \Delta H \\ \mathrm{ft} \end{gathered}$ | Reynolds Number |  |  | Flow Condition |  |
| 1 | 2 | 3 | 4 |  | 5 | 6 | 5 |
| 1 | 1.72 | 0.054 | 862 | 0.088 | 0.043 | Submerged | 11.26 |
| 2 | 4.47 | 0.088 | 2,240 | 0.088 | 0.113 | Submerged | 22.89 |
| 3 | 11.30 | 0.117 | 5,666 | 0.088 | 0.285 | Submerged | 50.26 |
| 4 | 26.31 | 0.156 | 13,192 | 0.088 | 0.663 | Submerged | 101.17 |
| 5 | 45.27 | 0.224 | 22,698 | 0.088 | 1.141 | Submerged | 145.33 |
| 6 | 58.54 | 0.276 | 29,352 | 0.088 | 1.475 | Submerged | 169.29 |
| 7 | 72.88 | 0.319 | 36,539 | 0.088 | 1.837 | Submerged | 196.18 |
| 8 | 139.38 | 0.692 | 69,882 | 0.088 | 3.513 | Submerged | 254.64 |
| 9 | 174.53 | 1.006 | 87,505 | 0.088 | 4.398 | Submerged | 264.36 |
| 10 | 212.65 | 2.299 | 106,621 | 0.088 | 5.359 | Submerged | 213.11 |
| 11 | 250.18 | 4.567 | 125,436 | 0.088 | 6.305 | Submerged | 177.88 |
| 12 | 325.53 | 10.526 | 163,216 | 0.088 | 8.204 | Submerged | 152.46 |
| Valve hysteresis tests |  |  |  |  |  |  |  |
| 1 | 103.60 | 0.444 | 51,944 | 0.088 | 2.611 | Submerged | 236.24 |
| 2 | 166.75 | 1.823 | 83,607 | 0.088 | 4.203 | Submerged | 187.64 |
| 3 | 139.53 | 1.164 | 69,957 | 0.088 | 3.516 | Submerged | 196.53 |
| 4 | 105.60 | 0.691 | 52,947 | 0.088 | 2.661 | Submerged | 193.05 |
| 5 | 122.25 | 0.792 | 61,295 | 0.088 | 3.081 | Submerged | 208.69 |
| Certified by: |  |  |  |  |  |  |  |
| $36$ |  | $1$ |  |  |  |  |  |
| Steven L. Barfuss P.E. |  |  |  |  |  |  |  |



Figure 3. Flow Rate vs Cv for the 4-inch WAPRO rubber check valve


Figure 4. Flow Rate vs Cv for the 4-inch WAPRO rubber check valve (hysteresis shown)

